Generalized model of thermal boundary conductance between SWNT and surrounding supercritical Lennard-Jones fluid – Derivation from molecular dynamics simulations –

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Abstract

Using classical molecular dynamics simulations, we have studied thermal boundary conductance (TBC) between a single-walled carbon nanotube (SWNT) and surrounding Lennard-Jones (LJ) fluids. With an aim to identify a general model that explains the TBC for various surrounding materials, TBC was calculated for three different surrounding LJ fluids, hydrogen, nitrogen, and argon in supercritical phase. The results show that the TBC between an SWNT and surrounding LJ fluid is approximately proportional to local density (ρ_L) formed on the outer surface of SWNT and energy parameter (ε) of LJ potential, and inverse proportional to mass (m) of surrounding LJ fluid. In addition, the influence of the molecular mass of fluid on TBC is far more than other inter-molecular potential parameters in realistic range of molecular parameters. Through these parametric studies, we obtained a phenomenological model of the TBC between an SWNT and surrounding LJ fluid.

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Nomenclature				
a	Proposed constant, kg m s ⁻¹ K ⁻¹			
С	Heat capacity, J kg ⁻¹ K ⁻¹			
ΔT	Temperature difference, K			
E_b	Total potential energy of the system, eV			
Κ	Thermal boundary conductance, MW $m^{\text{-2}}\text{K}^{\text{-1}}$			
k_b	Boltzmann's constant, J K ⁻¹			
L	Length of the respective tube, nm			
т	Mass, amu			
N	Number of molecules			
r	Distance, nm			
S	Contact area, nm ²			
T^*	Dimensionless temperature			
V_R	Repulsive force term			
V_A	Attractive force term			
V	Volume, nm ³			
Φ	Lennard-Jones potential, eV			
$ ho_{ m L}$	Local density, number of molecules nm ⁻³			
ρ	Density, kg m ⁻³			
$ ho^*$	Dimensionless density			
Е	Energy scale of LJ potential, eV			
σ	Length scale of LJ potential, nm			
τ	Relaxation time constant, ps			
v	Velocity, m s ⁻¹			

Subscript

С	Carbon
SWNT	Single-walled carbon nanotube
LJ	Surrounding LJ fluid molecules
SWNT-LJ	Inter material property between an SWNT and LJ fluid
MD	Molecular dynamics simulation
model	The obtained model

1. Introduction

Single-walled carbon nanotubes (SWNTs) [1] have been investigated in various fields to take advantage of their outstanding electrical, optical, mechanical and thermal properties [2,3]. In thermal engineering, their thermal conductivity that is believed to surpass even the value of diamond has caught particular attention. One of the promising applications is to use SWNTs as additives to enhance thermal conductivity of composite materials [4-8]. For instance, the thermal conductivity enhancement by adding nanotube in oil has been measured to be much higher than the enhancement predicted by theoretical models based on Fourier's law of heat conduction [9]. In addition, SWNTs have been shown to augment thermal conductivity of epoxy more than larger-diameter carbon fibers [10]. On the other hand, it is known that the effective thermal conductivity of the composite can be strongly influenced by thermal boundary resistance (TBR) between carbon nanotubes and surrounding medium [11, 12]. Therefore, to quantify the heat flow through the system for thermal management, it is essential to understand TBR.

Thermal boundary resistance, with its importance in small scale, has been studied by various methods and viewpoints. Since convectional models such as acoustic mismatch model (AMM) and diffuse mismatch model (DMM) fail to accurately predict TBR [13], molecular dynamics simulations, with capability of resolving the atomistic structure and dynamics at the interface, have been widely used. One of the first works was reported by Maruyama and Kimura [14] who demonstrated that temperature discontinuity resulting from thermal resistance exists at the solid-liquid surface, so-called Kapitza resistance. This was followed by Ohara and Suzuki [15] who investigated interfacial thermal resistance at a solid-liquid surface based on the intermolecular energy transfer. There have been also several researches on TBR between SWNT and surrounding material [16-19]. For the interface between SWNT and octane liquid, Shenogin et al. [16] demonstrated the TBR plays a barrier to thermal conductivity for carbon-nanotube polymer composite and organic suspensions. Furthermore, Carlborg et al. [17] investigated the TBR between SWNT and Lennard-Jones molecules focusing on the frequency dependence of energy transport. Hu et al. [18] showed the TBR between SWNT and air with the influence of energy parameter of LJ potential. While these studies have revealed interfacial thermal transport of specific system or parameter, the general model that relates TBR and molecular potential parameters, which would be useful to design SWNT composites, is not available to this date.

In this study, we investigate the interfacial thermal transport between an SWNT and various surrounding LJ fluids with the aims to identify the general scaling law by exploring a wide range of parameter space. Here, we qualify the interfacial thermal transport in terms of thermal boundary conductance (TBC), the reciprocal of the TBR. The effect of various fluid parameters was investigated using non-stationary MD simulation, to resolve atomic-scale dynamics between an SWNT and surrounding LJ fluid such as argon, hydrogen, and nitrogen in the supercritical phase.

2. Simulation Method

A 25.1-nm-long SWNT consisting of 2000 carbon atoms was placed in the center of a rectangular simulation cell and surrounded by fluid of 1280 molecules, as shown in Fig. 1. Simulations were conducted for an armchair SWNT with chirality (5, 5), which has a radius of 0.69 nm. The cross-sectional area of the simulation cell was varied from 2.3×2.3 nm to 46.0×46.0 nm and periodic boundary conditions were applied in all directions.

We employed the Brenner potential [20] with a simplified form [21] to describe the carbon-carbon interactions within the SWNT as the total potential energy of the system E_b , which is expressed as the sum of the binding energy of each bond between carbon atoms *i* and *j*.

$$E_b = \sum_i \sum_{j(i(1)$$

 $V_R(r_{ij})$ and $V_A(r_{ij})$ are the repulsive and attractive force terms, respectively, which take the Morse-type form with a cutoff function. B_{ij} * represents the effects of the bonding condition of the atoms. We employed the parameter set II, which is known to be better at reproducing the carbon-carbon force constant [20].

For the interaction between carbon and the surrounding LJ fluid, we adopted the 12-6 Lennard-Jones (LJ) potential based on Van der Waals forces between surrounding fluids molecules,

$$\Phi(r_{ij}) = 4\varepsilon \left[\left(\frac{\sigma}{r_{ij}} \right)^{12} - \left(\frac{\sigma}{r_{ij}} \right)^{6} \right], \qquad (2)$$

where ε and σ are the energy and length scales and r_{ij} is the distance between *i* and *j* molecules. The LJ parameters used are shown in Table 1 [19,22,23]. We determined $\varepsilon_{SWNT-LJ}$ and $\sigma_{SWNT-LJ}$ at the interface between SWNT and surrounding LJ fluid by the Lorentz-Berthelot mixing rules as follows.

$$\varepsilon_{\text{SWNT-LJ}} = \sqrt{\varepsilon_{\text{C}} \varepsilon_{\text{LJ}}} . \tag{3}$$

$$\sigma_{\text{SWNT-LJ}} = \frac{(\sigma_{\text{C}} + \sigma_{\text{LJ}})}{2} . \tag{4}$$

The cutoff distance of the LJ potential function was set to $3.5\sigma_{LJ}$, and the velocity Verlet method [24] was adopted to integrate the equation of motion with a time step of 0.5 fs. The temperature was defined by assuming the local equilibrium,

$$\sum_{i}^{N} \frac{1}{2} m v_{i}^{2} = \frac{3}{2} N k_{B} T , \qquad (5)$$

where m, N, v_i , k_B and T are mass, number of molecules, velocity of molecule i, Boltzmann

constant, and temperature, respectively. The temperature was controlled by the velocity scaling method.

In this research, we setup the simulation with dimensionless temperature $T^* = k_B T / \varepsilon_{I,I}$, and dimensionless density $\rho^* = \rho \sigma_{IJ}^3/m$. Since the intrinsic heat-conduction resistance of SWNT and fluid is sufficiently small compared to the SWNT-LJ fluid TBR, the heat transfer problem can be simplified to interfacial resistance between two point masses with certain heat capacities and thus, we employed the lumped-heat-capacity method. The density ρ^* is varied from 0.001 to 0.3 by adjusting the cell size of the unit cell. When setting up the density ρ^* , changing the cell size or increasing the number of fluid molecules did not considerably affect the results. In each case, the first step was to keep the SWNT and surrounding LJ fluid at a fixed temperature for 10 ps. The system was then equilibrated for 990 ps without temperature control. After 1000 ps, the SWNT was heated instantaneously from $T^*=3.0$ to 4.5. Note that the temperature of the system was always kept to be above critical temperature of bulk LJ system [25]. Figure 2 shows the result of a simulation with argon of $\rho^*=0.04$ in a 7.0×7.0×25.1 nm cell, and the relaxation time in this case was 300 ps. Variations in the SWNT and surrounding LJ fluid temperature were then recorded. The ensemble-average was obtained from five independent simulations with different initial conditions. By fitting the temperature difference with $\Delta T = \Delta T_0 \exp(-t/\tau)$, we obtain the relaxation time τ . Then, the thermal boundary conductance K can be calculated as

$$K = \left[\left\{ \frac{1}{\rho_{\text{SWNT}} c_{\text{SWNT}} V_{\text{SWNT}}} + \frac{1}{\rho_{\text{LJ}} c_{\text{LJ}} V_{\text{LJ}}} \right\} \tau S \right]^{-1}, (6)$$

where ρ , *c*, *V* and *S* are density, heat capacity, volume and contact area, respectively [17]. The subscripts SWNT and LJ refer to the SWNT and surrounding LJ fluid. The contact area *S* was calculated as $S=\pi L(d+\sigma_{SWNT-LJ})$, where *d* is the diameter of the (5, 5) SWNT, $\sigma_{SWNT-LJ}$ is length parameter at interface between SWNT and surrounding LJ fluid, and *L* is the length of the SWNT.

3. Results and Discussion

3.1 Density dependence of thermal boundary conductance

The TBC between an SWNT and various surrounding LJ fluids was calculated over a wide density range. The density and fluid dependences of TBC are shown in Fig. 3. Note that the data are plotted on a log-log scale. The TBC of SWNT-hydrogen case was higher than other fluids for all calculated densities, whereas nitrogen and argon have almost the same TBC values, ranging from 0.037 to 1.27 MW/m²K. It can be seen that, for all the tested fluids, TBC show

nonlinear dependence on the dimensionless density with a kink at around $\rho^*=0.04$, which cannot be explained by the phase transition as the simulations were performed for supercritical fluids.

Now we consider the local fluid density, which is the number density of LJ molecules in the first adsorption layer surrounding the SWNT. The maximum value of the density in the first adsorption layer is termed ρ_L . As seen from the radial distribution functions shown in Fig. 4, the local density of each fluid ρ_L increases with dimensionless density ρ^* . The distance between the first adsorption layer and the SWNT is different for each fluid, and this distance depends on the value of $\sigma_{SWNT-LJ}$ shown in Table 1. Although the second layer was begun to be observed at higher ρ^* , the peak density of the layer was so small that it was considered to have negligible influence on the TBC. The molecules exhibited no noticeable layering beyond the second layer.

Figure 5 shows how the TBC depends on ρ_L of each fluid. The TBC increases linearly with ρ_L , and the hydrogen case is found to be much more sensitive to ρ_L than argon or nitrogen. By comparing Fig. 4 and Fig. 5 we found that the difference in sensitivity should originate from other inter molecular parameters, which are explored in the next section.

3.2 Fluid dependence of thermal boundary conductance

The parameters used in the simulations were energy scale ε , length scale σ and mass *m*, as seen in Table 1 and Table 2. In order to determine the effect of each parameter on determining the thermal boundary conductance, we have calculated TBC for systems with hypothetical fluids with parameters varied in realistic range. With argon parameters as standard values, each parameter was varied by keeping the other two constant. For all the cases, ρ^* was kept at 0.04.

Firstly, Figure 6(a) shows the relationship between ε_{LJ} and TBC. The TBC increases from 0.19 to 0.54 MW/m²K as ε_{LJ} increases from 3.18 to 10.34 meV. Secondly, we investigated the effect of σ_{LJ} . As seen in Fig. 6(b), the change in TBC, which ranges from 0.54 to 0.72 MW/m²K, is smaller than in the case of ε_{LJ} (Fig. 6(a)). Lastly, we evaluated the effect of m_{LJ} . As seen in Fig. 6(c), we found that the TBC was inverse-proportional to the mass. The dependence of ε_{LJ} , σ_{LJ} and m_{LJ} were fitted by $K \propto \varepsilon_{LJ}^{0.9}$, $K \propto \sigma_{LJ}^{-1.34}$ and $K \propto m_{LJ}^{-0.76}$, respectively.

3.3 Generalized model of thermal boundary conductance

Through the above parametric studies, we obtained a phenomenological description of the thermal boundary conductance between an SWNT and surrounding LJ fluid, described by

$$K_{\text{model}} = a \cdot \frac{\rho_{\text{L}} \cdot \varepsilon_{\text{LJ}}}{m_{\text{LJ}}}$$
(7)

where a is equal to 1.03×10^{-30} kg m s⁻¹K⁻¹. The effects of ε_{LJ} and m_{LJ} of thermal boundary

conductance are simplified from the fitted relations $\varepsilon_{LJ}^{0.9}$ and $m_{LJ}^{-0.76}$, as seen in the insets in Fig. 6(a) and Fig. 6(c), respectively. Here, we omitted the σ_{LJ} from the model because of the weak dependence of TBC on σ_{LJ} in the realistic range, as shown in the inset in Fig. 6(b). We verified the accuracy of the Eq. (7) by comparing values of the TBC with those obtained from MD simulation (Fig. 7), and they show high consentaneity. However, the values of TBC for two-nitrogen and one-argon cases taken in lower densities seem the TBC obtained from MD is much higher than that from Eq. (7). We believe they should be clarified with more elaborate physical mechanism for heat transfer between SWNT and surrounding fluid in future.

4. Conclusion

The thermal boundary conductance *K* between a single-walled carbon nanotube (SWNT) and various surrounding Lennard-Jones (LJ) fluids was investigated using non-stationary molecular dynamics simulations. We found that the density dependence on thermal boundary conductance is proportional to the local density of the molecules in the first adsorption layer. The hydrogen case is found to be much more sensitive to the local density than argon or nitrogen. This comes from that dependence of TBC on fluid molecular parameters, where TBC is approximately proportional to energy scale (ε) of LJ potential, and inverse proportional to mass (*m*) of surrounding LJ fluid. The molecular mass was found to influence TBR far more than other fluid parameters (i.e., ε and σ) within the realistic parameter ranges. Through the parametric studies, we have obtained a phenomenological model of the thermal boundary conductance between an SWNT and surrounding LJ fluid and verified the accuracy of the model.

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Tables

	ε (meV)	$\sigma(\text{nm})$
C – C [19]	2.12	0.337
Ar – Ar [19]	10.33	0.340
$H_2 - H_2$ [22]	3.18	0.293
$N_2 - N_2$ [23]	8.54	0.359
Ar-SWNT	4.67	0.338
$H_2 - SWNT$	2.59	0.315
$N_2 - SWNT$	4.25	0.348

Table 1. Parameters of Lennard-Joned fluid.

Table 2. Mass of Lennard-Jones fluid.

	С	Ar	H_2	N_2
m (amu)	12.0	39.95	2.02	28.01

Figure Captions

Figure 1. Snapshot of a typical molecular dynamics simulation of argon with dimensionless density $\rho^*=0.04$.

Figure 2. (a) Temperature time history for SWNT and surrounding LJ fluid, and (b) temperature difference between the SWNT and argon for $\rho^*=0.04$.

Figure 3. Density dependence of thermal boundary conductance between SWNT and surrounding LJ fluids.

Figure 4. Radial distribution functions of (a) argon, (b) hydrogen and (c) nitrogen for different values of ρ^* .

Figure 5. Correlation between local density and thermal boundary conductance.

Figure 6. The effect of each parameter (a) energy scale ε_{LJ} (b) length scale σ_{LJ} and (c) mass m_{LJ} on determining the thermal boundary conductance. Corresponding insets show the difference in TBC resulting from using approximated relations. All cases are performed at $\rho^*=0.04$.

Figure 7. Comparison of thermal boundary conductance values obtained from MD simulation and Eq.(7).



Fig. 1







Fig. 3



Fig. 4



Fig. 4



Fig. 5



Fig. 6



Fig. 6



Fig. 7